

SIMULATION OF WATER-SALT DYNAMICS OF SOIL ROOTS, SUBSOIL AND SUBSOIL LAYERS

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Annotation

In the article, the creation of a mathematical model of the process of water-salt exchange during the cultivation of cotton on soils prone to salinization due to the growing shortage of irrigation water.

Key words: Water deficit, water resources, technology, water conservation, water-salt, mathematical model.

One of the unique aspects of the 21st century is the rapid growth of water consumption in various aspects of the national economy. Irrigated farming is taking the first place in this field. Moisture resources, soil fertility, and applied agrotechnics determine the natural biological productivity in different natural and climatic conditions of the world.« The introduction of computer technology as a tool for rapid calculation of physical processes occurring in the "soil-water-plant" system allows to predict the productivity of agroecosystems in a short period of time based on mathematical modeling.

The limitation of water resources is increasingly demanding science-based methods that predict changes in humidity, taking into account the applied agrotechnical and reclamation measures.

The summation of works aimed at prevention of irrigation water deficiency and drought prevention and the accuracy of

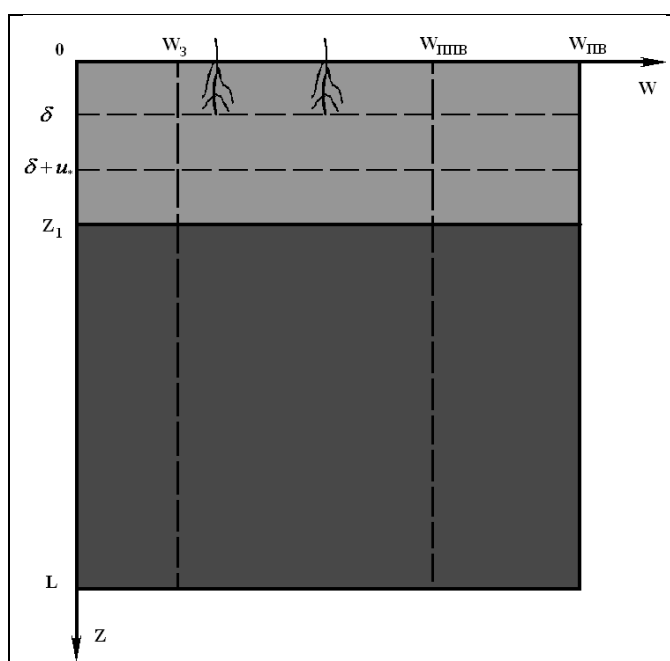


Figure 1 Schematic section of soil
 $0 \leq z \leq \delta + u$ – root layer; $0 \leq z \leq z_1$ – arable layer; $z_1 \leq z \leq L$ – plowed sub-layer

external countermeasures depend on accurate and reliable prediction of moisture dynamics of the irrigated area. In this article, WZ humidity to WPV. changes in volumetric humidity up to relative absolute humidity were calculated. If the cross-section of the medium under consideration (Fig. 1) consists of three layers: the root layer, the arable layer and the arable sub-layer, the moisture migration is expressed by the following equation [1, 2, 3]:

$$\left\{ \begin{array}{l} \frac{d}{dz} \left[D_1(W_1) \frac{dW_1}{dz} \right] - \frac{dK_1}{dz} - \frac{12E_T}{7(\delta + u_*)} \left[1 - \frac{z}{2(\delta + u_*)} - \frac{z^2}{2(\delta + u_*)^2} \right] = 0, \quad (0 \leq z \leq \delta + u_*) \\ \frac{d}{dz} \left[D_1^*(W_1^*) \frac{dW_1^*}{dz} \right] - \frac{dK_1^*}{dz} = 0, \quad (\delta + u_* \leq z \leq z_1) \\ \frac{d}{dz} \left[D_2(W_2) \frac{dW_2}{dz} \right] - \frac{dK_2}{dz} = 0, \quad (z_1 \leq z \leq L) \end{array} \right. \quad (1.1)$$

$$W_1(z)|_{z=0} = W_{IP} = const; \quad (1.2)$$

$$W_1(\delta + u_*) = W_1^*(\delta + u_*);$$

$$\left[K_1(W_1) - D_1(W_1) \frac{dW_1}{dz} \right]_{z=\delta+u_*} = \left[K_1^*(W_1^*) - D_1^*(W_1^*) \frac{dW_1^*}{dz} \right]_{z=\delta+u_*}; \quad (1.3)$$

$$W_1^*(z_1) = W_2(z_1) \quad (1.4)$$

$$\left[K_1^*(W_1^*) - D_1^*(W_1^*) \frac{dW_1^*}{dz} \right]_{z=z_1} = \left[K_2(W_2) - D_2(W_2) \frac{dW_2}{dz} \right]_{z=z_1} \quad (1.5)$$

$$W_2(L) = W_{IB} = const \quad (1.6)$$

W_1, W_2 – volumetric humidity; moisture transfer coefficients are accepted in the following form:

$$K_1(W_1) = A_1 e^{A_2 z}; \quad K_1^*(W_1^*) = A_1^* e^{A_1^* z}; \quad K_2(W_2) = B_1 e^{B_2 z};$$

Instead of diffusivity coefficients, their average values were used

$$D_1(W_1) = D_1 = const \quad D_1^*(W_1^*) = D_1^* = const \quad D_2(W_2) = D_2 = const;$$

δ – the depth of the root system; $\delta + u^*$ is the depth at which plant roots can absorb moisture; z_1 – granitic medu pahotnym and subpahotnym layer; W_{pr} – some intermediate moisture content between the moisture content of W_3 and the boundary moisture content W_{ppv} , i.e.

$$W_3 < W_{pr} < W_{ppv};$$

L – the depth of the underground water level; W_{pv} – total moisture capacity; Z – a vertical coordinate pointing down from the earth's surface [4].

Here the following condition is fulfilled

$$\frac{12E_T}{7(\delta + u_*)} \int_0^{\delta+u_*} \left[1 - \frac{z}{2(\delta + u_*)} - \frac{z^2}{2(\delta + u_*)^2} \right] dz = E_T$$

In this case, it should be taken into account that the volumetric moisture in the plowed layer can only be in the following inequality

$$W_3 \leq W \leq W_{ppv},$$

here, $e W_3$ – humidity; W_{ppv} – the limit of field humidity. (1) Integrating each equation of the system of equations twice, we form the following expression:

$$\frac{dW_1}{dz} - \frac{A_1}{D_1} e^{A_2 z} - \frac{A_5}{D_1} \left[z - \frac{z^2}{4(\delta + u_*)} - \frac{z^3}{6(\delta + u_*)^2} \right] = C_5, \quad (1.7)$$

here $A_5 = \frac{12E_T}{7D_1(\delta + u_*)}$,

$$W_1(z) = \frac{A_1}{A_2 D_1} e^{A_2 z} - \frac{A_5}{D_1} \left[\frac{z^2}{2} - \frac{z^3}{12(\delta + u_*)} - \frac{z^4}{24(\delta + u_*)^2} \right] + C_5 z + C_6 \quad (1.8)$$

(1) Interpolating the second and third equations of the system of equations, we form the following expression:

$$\frac{dW_1^*}{dz} - \frac{A_1^*}{D_1^*} e^{A_2^* z} = C_7 \quad \text{или} \quad W_1^*(z) = \frac{A_1^*}{A_2^* D_1^*} e^{A_2^* z} + C_7 z + C_8 \quad (1.9)$$

$$\frac{dW_2}{dz} = \frac{B_1}{D_2} e^{B_2 z} + C_9, \quad W_2(z) = \frac{B_1}{B_2 D_2} e^{B_2 z} + C_9 z + C_{10} \quad (1.10)$$

Given the boundary conditions, we determine S_5, S_6, S_7, S_8, S_9 and S_{10} :

$$C_5 = \frac{D_1^* D_2 \Phi}{P} \quad C_6 = W_{pp} - \frac{A_1}{A_2 D_1} \quad C_7 = \frac{D_1 D_2 \Phi}{P} + \frac{7A_5 U}{12D_1^*},$$

$$C_8 = W_{pp} + \frac{A_1}{A_2 D_1} [e^{A_2 U} - 1] - \frac{3A_5 U^2}{8D_1} - \frac{A_1^*}{A_2^* D_1^*} e^{A_2^* U} + U \left[D_2 (D_1^* - D_1) \frac{\Phi}{P} - \frac{7A_5 U}{12D_1^*} \right]$$

$$C_9 = \frac{D_1 D_1^* \Phi}{P} + \frac{7A_5 U}{12D_2} \quad C_{10} = W_{pb} - \frac{B_1}{B_2 D_2} e^{B_2 L} - L \left[D_1 D_1^* \frac{\Phi}{P} + \frac{7A_5 U}{12D_2} \right] \quad (1.11)$$

here $U = \delta + u_*$ $P = D_1 D_2 (z_1 - U) + D_1^* D_2 U + D_1^* D_1 (L - z_1)$

$$\Phi = W_{pb} - W_{pp} - \frac{B_1}{B_2 D_2} [e^{B_2 L} - e^{B_2 z_1}] - \frac{A_1^*}{A_2^* D_1^*} [e^{A_2^* z_1} - e^{A_2^* U}] - \frac{A_1}{A_2 D_1} [e^{A_2 U} - 1] + \frac{3A_5 U^2}{8D_1} - \frac{7A_5 U}{12D_1} \left[\frac{z_1 - U}{D_1^*} - \frac{L - z_1}{D_2} \right] \quad (1.12)$$

Substituting all the derivative constants found into $C_j = (j = \overline{5,10})$, we determine the volume moisture distribution as a function of depth:

$$W_1(z) = W_{pp} + \frac{A_1}{A_2 D_1} [e^{A_2 z} - 1] + \frac{A_5 z^2}{D_1} \left[\frac{1}{2} - \frac{z}{12U} - \frac{z^2}{24U^2} \right] + D_1^* D_2 \frac{\Phi}{P} z$$

$$0 \leq z \leq \delta + u_*$$

$$W_1^*(z) = \frac{A_1^*}{A_2^* D_1^*} \left[e^{A_2^* z} - e^{A_2^* (\delta + u_*)} \right] + z \left[D_1 D_2 \frac{\Phi}{P} + \frac{7A_5 (\delta + u_*)}{12D_1^*} \right] + \frac{A_1}{A_2 D_1} (e^{A_2 (\delta + u_*)} - 1) + W_{IP} - \frac{3A_5}{8D_1} (\delta + u_*)^2 + \left[(D_1^* - D_1) D_2 \frac{\Phi}{P} - \frac{7A_5 (\delta + u_*)}{12D_1^*} \right] (\delta + u_*) \quad ; (1.13)$$

$$\delta + u_* \leq z \leq z_1$$

$$W_2(z) = W_{IB} - \frac{B_1}{B_2 D_2} (e^{B_2 L} - e^{B_2 z}) + (L - z) \left[D_1 D_1^* \frac{\Phi}{P} + \frac{7A_5 (\delta + u_*)}{12D_2} \right]$$

$$z_1 \leq z \leq L$$

Figure 2 shows the above equation graphically

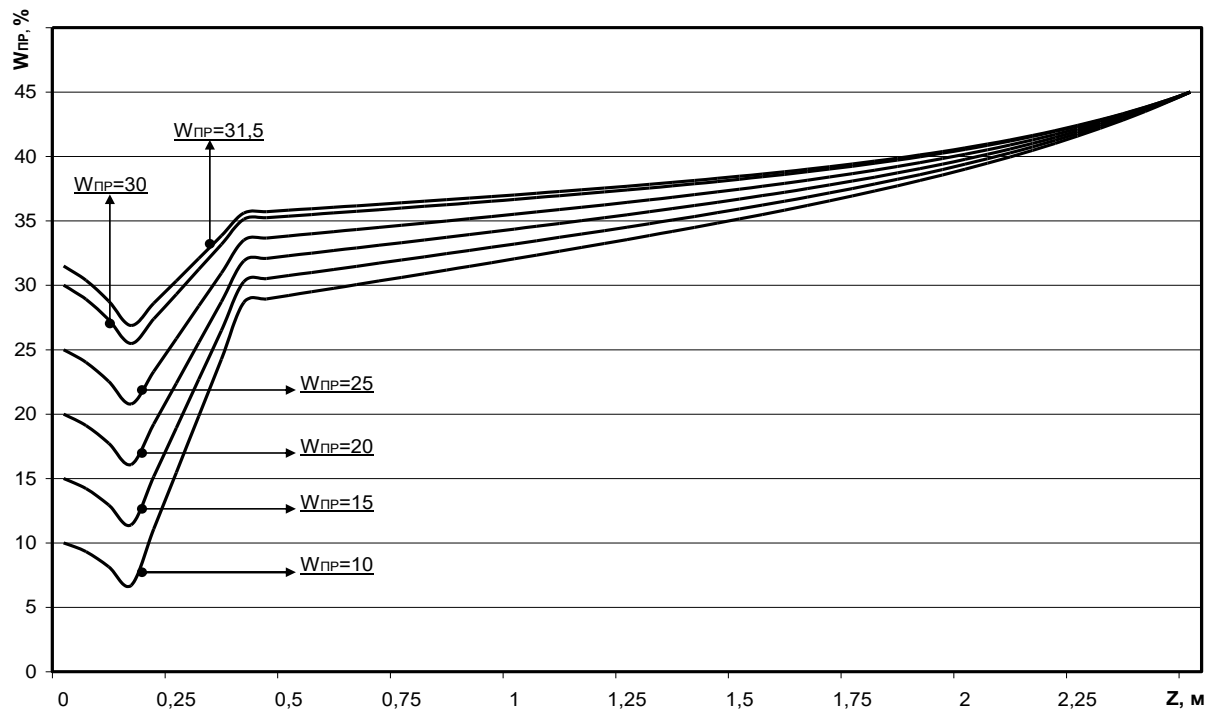


Figure 2. Graph of the equation $W_{PR} = f(z)$ for desert conditions (Syrdarya region, Mirzaabad district) $(\delta + u_*) = 0.15$ m, $Z_I = 0.4$ m.

As the analysis of graph indicators shows, the conducted theoretical studies have reliable similarities with the natural data of these processes. The developed moisture transport models are suitable for three-layered environments and take into account soil porosity, groundwater level, and infiltration and transpiration. Authors' comparison of theoretical results with experimental data made it possible to clarify the parameters of equations (1,3). The results are presented in the table below.

coefficients of mathematical models.**1.1- Table**

The location of the object	Lower Chirchik region	Zomin	Mirzaabad district	Kattakorgon	Nishan district	Kumkorgon district	Kuva District	Sardoba District	
SIU	Sayram water	Winner water	Yangiabad	Madatsuv-JRK	Triangle	N. Mirzaev	Akbarabad	G'. Ghulam	
Mechanical composition	Sandy	Heavy sand	Heavy sand	Heavy sand	Medium grainy	Medium grainy	Lightly creamy	Lightly creamy	
Equation coefficients	A_1	$9.39 \cdot 10^{-4}$	$3.29 \cdot 10^{-4}$	$2.18 \cdot 10^{-4}$	$2.023 \cdot 10^{-4}$	$5.44 \cdot 10^{-4}$	$2.31 \cdot 10^{-4}$	$3.64 \cdot 10^{-3}$	$3.32 \cdot 10^{-3}$
	A_1^*	$7.83 \cdot 10^{-4}$	$4.51 \cdot 10^{-4}$	$7.34 \cdot 10^{-5}$	$2.21 \cdot 10^{-4}$	$1.08 \cdot 10^{-4}$	$9.28 \cdot 10^{-5}$	$4.28 \cdot 10^{-3}$	$3.68 \cdot 10^{-3}$
	A_2	1,94	2.01	1.73	1.56	2,23	2,4	2,31	2,2
	A_2^*	1,94	1.49	1.57	1.84	2,73	2,65	2,44	2,1
	B_1	$2.7 \cdot 10^{-3}$	$4.6 \cdot 10^{-4}$	$3.44 \cdot 10^{-4}$	$1.66 \cdot 10^{-4}$	$2.27 \cdot 10^{-4}$	$1.52 \cdot 10^{-4}$	$5.17 \cdot 10^{-3}$	$3.71 \cdot 10^{-3}$
	B_2	1,562	2.31	2.517	2.44	2,43	2,65	1,828	2,088
	D_1	0.005	0.0037	0.0044	0.0052	$6.85 \cdot 10^{-3}$	$5.5 \cdot 10^{-3}$	$3.98 \cdot 10^{-3}$	0.003
	D_1^*	0.0011	0.00086	0.00093	0.0012	$1.05 \cdot 10^{-3}$	$9.5 \cdot 10^{-4}$	$4.81 \cdot 10^{-4}$	0.0005
D_2	0.022	0.01	0.017	0.023	$12.4 \cdot 10^{-3}$	$19.1 \cdot 10^{-3}$	$6.84 \cdot 10^{-3}$	0.008	

The obtained information provides the means of optimal determination of the completeness of the soil step by step. direct, complete. The information in the table shows that volume reduction affects settlement, horizontal renaissance, and access to the mechanical structure of the soil. The large difference between the coefficients of the same type of soil is explained by both chemical composition and climatic conditions.

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